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DEGLI STUDI
DI PADOVA

High fidelity simulations of high-speed flows for aerospace problems

Michele Cogo - 37th Cycle

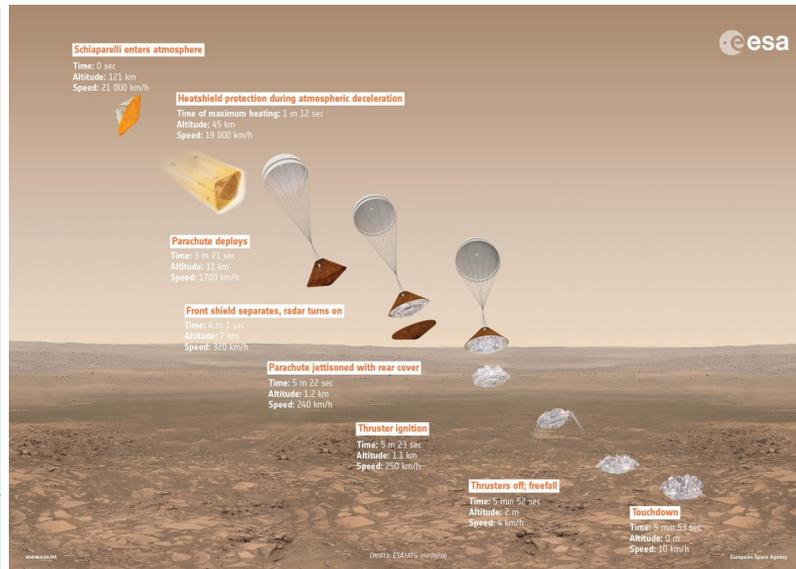
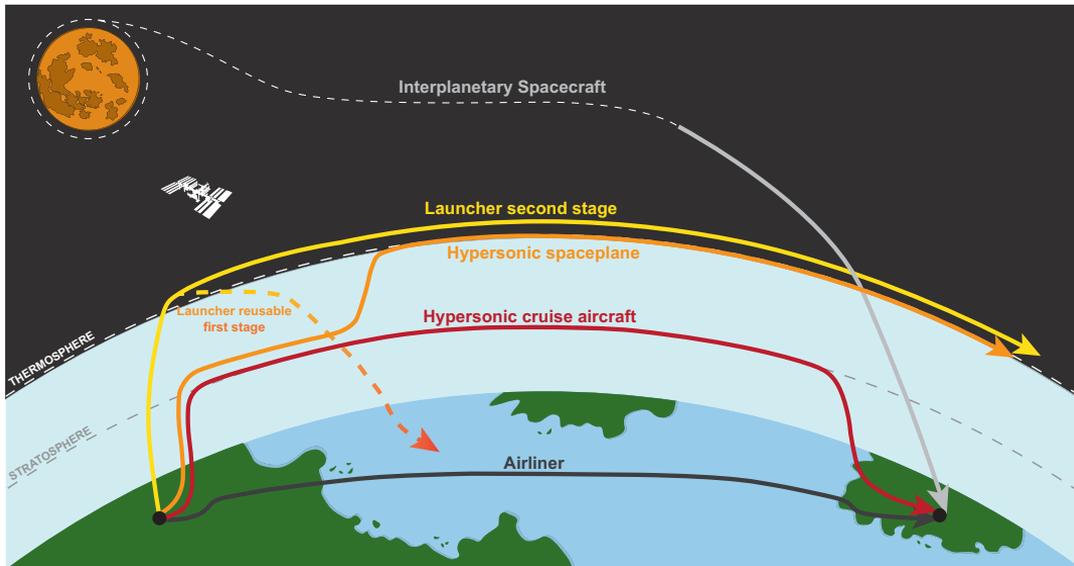
Supervisor: Prof. Francesco Picano

Admission to the final exam - 17/09/2024

High-speed flows:

Flight trajectories on Earth...

...and reentry on Mars

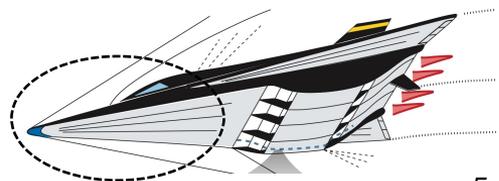


ESA website

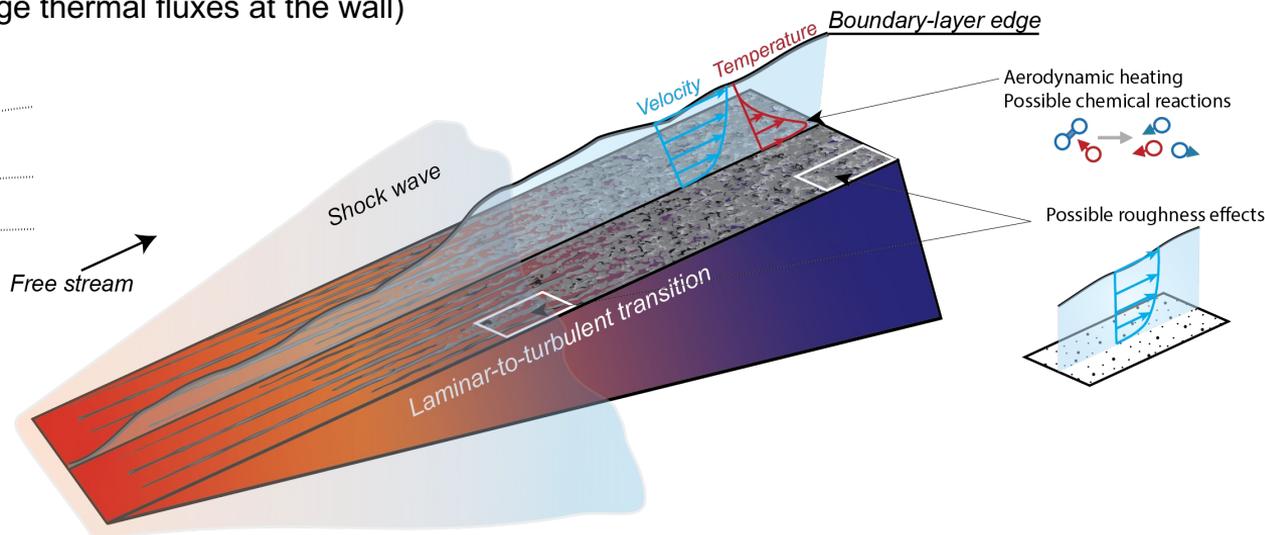
Main features of high-speed flight at low altitudes:

- High Reynolds number (turbulent boundary layers)
- High freestream Mach numbers (intense shocks and large recovery temperatures) →
- Possible chemical-reactions activated by high temperatures
- Aerodynamic heating (large thermal fluxes at the wall)

The presence of turbulent, hot and highly compressible boundary layers increase the mechanical and thermal loads on the vehicle!



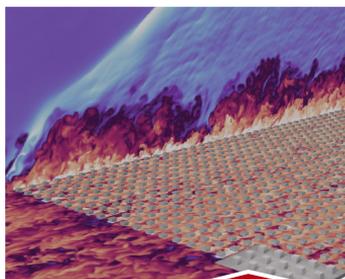
Adapted from Urzay et al., 2018, Annu. Rev. Fluid Mech.



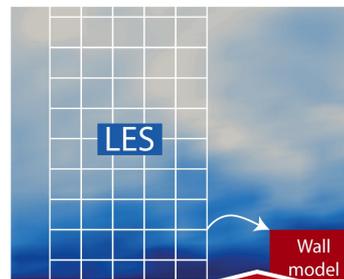
Three main tasks:



High-speed boundary layers over smooth walls



High-speed boundary layers over rough walls



Wall-models for hypersonic boundary layers

In collaboration with:



SAPIENZA
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TU Delft



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Objectives of this study:

1. Direct Numerical Simulations of high-speed turbulent boundary layers over smooth walls (Task #1)
2. Direct Numerical Simulations of high-speed turbulent boundary layers over rough walls (Task #2)
3. Wall-models for hypersonic turbulent boundary layers with chemical reactions (Task #3)

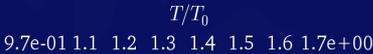
How are turbulent flows modelled?

DNS

LES

RANS

COMPUTATIONAL COST



- Solves the spatially averaged N-S equations
- Large eddies are directly resolved, smaller-than-mesh eddies are modeled
- Less expensive than DNS, but still unpractical for industrial applications (especially for bounded flows)



- Solves time-averaged N-S equations
- All turbulent length scales are modeled
- Most widely used approach for industrial flows

PHYSICAL ACCURACY

No model!
 $\Delta x \simeq \eta$

Modelling small scales
 $\eta < \Delta x < L_0$

Modelling all scales
 $\Delta x \simeq L_0$

Large-Eddy Simulation

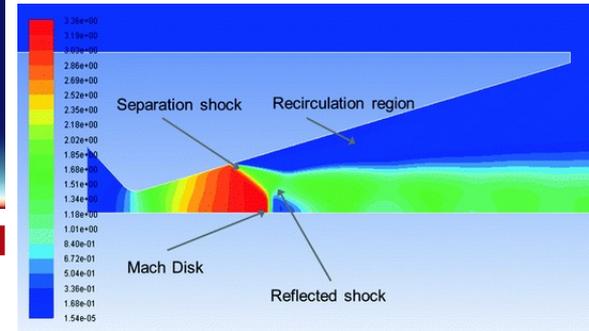
Entry #: V034

Large-eddy simulation of an over-expanded nozzle

Britton J Olson
Sanjiva K Lele

APS 2011
Division of Fluid Dynamics
Baltimore, MD

Reynolds-Averaged Navier-Stokes simulation



| Solver | Numerical method | Immersed boundary method |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <p><u>STREAMS</u> (Bernardini et al. CPC 2021):</p> <ul style="list-style-type: none"> Open-source numerical solver for compressible flows Supports MPI parallelization and multi-GPU architectures | <p><u>Direct Numerical Simulation:</u></p> <ul style="list-style-type: none"> Navier-Stokes equations are solved with very high temporal and spatial resolution, down to the Kolmogorov scale No model is employed | <ul style="list-style-type: none"> Numerical method capable of representing the solid boundary on structured cartesian grids Ghost-Point-Forcing Method -> the mesh nodes inside the solid boundary are used as ghost points to give the right boundary conditions (Piquet et al. [2016]) |

Navier-Stokes equations in the conservative formulation:

$$\frac{\partial \mathbf{U}}{\partial t} = - \frac{\partial \mathbf{F}_j(\mathbf{U})}{\partial x_j} + \frac{\partial \mathbf{F}_{vj}(\mathbf{U})}{\partial x_j}$$

$$\mathbf{U} = \begin{bmatrix} \rho \\ \rho u_j \\ \rho E \end{bmatrix} \quad \mathbf{F}_{vj}(\mathbf{U}) = \frac{\sqrt{\gamma} M_\infty}{Re} \begin{bmatrix} 0 \\ \sigma_{ij} \\ \sigma_{ij} u_j - \frac{1}{Pr} \frac{\gamma}{\gamma-1} q_j \end{bmatrix} \quad \mathbf{F}_j(\mathbf{U}) = \begin{bmatrix} \rho u_j \\ \rho u_i u_j + p \delta_{ij} \\ \rho u_j H \end{bmatrix}$$

Calorically-perfect gas:

$$E = c_v T + u_i u_i / 2$$

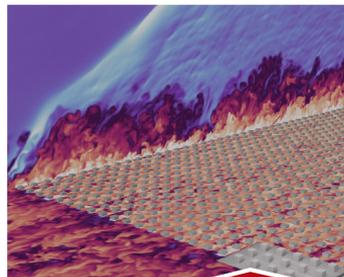
$$H = E + p / \rho$$

$$p = \rho T$$

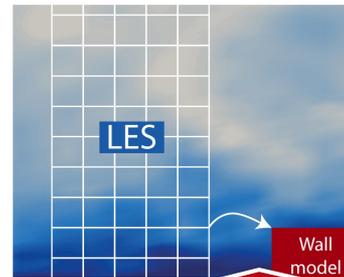
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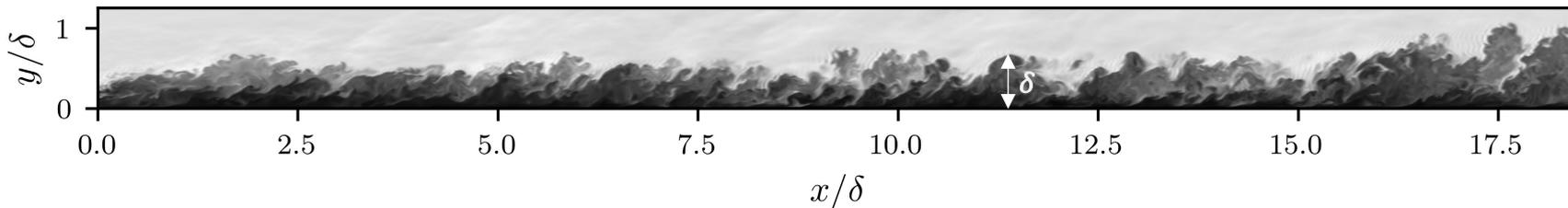
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High-speed boundary layers are a representative of the thin region near the aircraft surface. Their study is of critical importance for estimating the drag and heat transfer experienced by the vehicle.

Key parameters of the study:

$$M_\infty = u_\infty / a_\infty$$

Mach number

$$Re_\tau = \bar{\rho}_w u_\tau \delta / \bar{\mu}_w$$

Friction Reynolds number

$$T_w$$

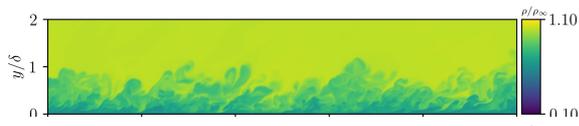
Wall temperature

Large variations of thermodynamic properties (e.g. density)

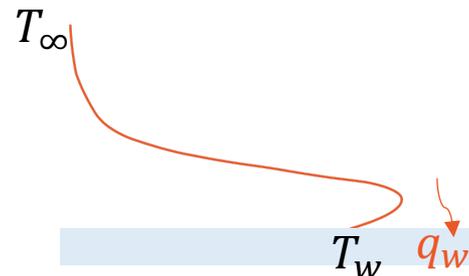
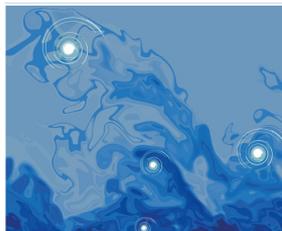
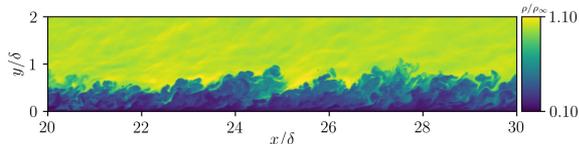
Greater separation of turbulent scales

Large wall heat fluxes (aerodynamic heating)

$M_\infty = 2$



$M_\infty = 6$



Visualization of Q-criterion at Mach 6



First study:

Effect of **Reynolds** and **Mach** numbers on high-speed zero-pressure-gradient turbulent boundary layers

Key points discussed:

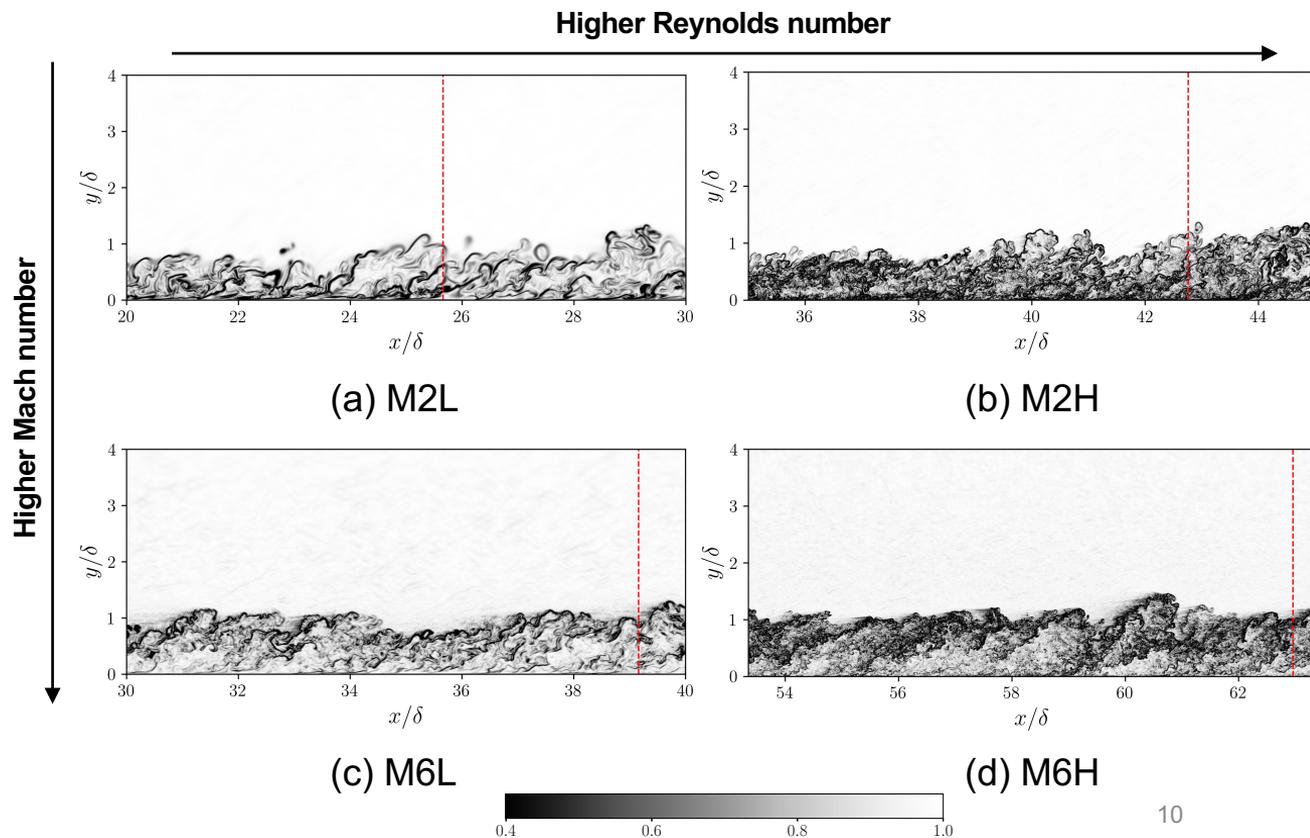
- Correlation between velocity and temperature fluctuations
- Uniform momentum and temperature zones
- Validity of compressibility transformations and temperature-velocity relations
- Spatial organization and length scales

Database:

- $M_\infty = 2, 6$
- $Re_\tau = 450, 1950$

Michele Cogo

Contours of the density gradient in a streamwise wall-normal plane



Contours of density in a streamwise wall-normal plane

Second study:

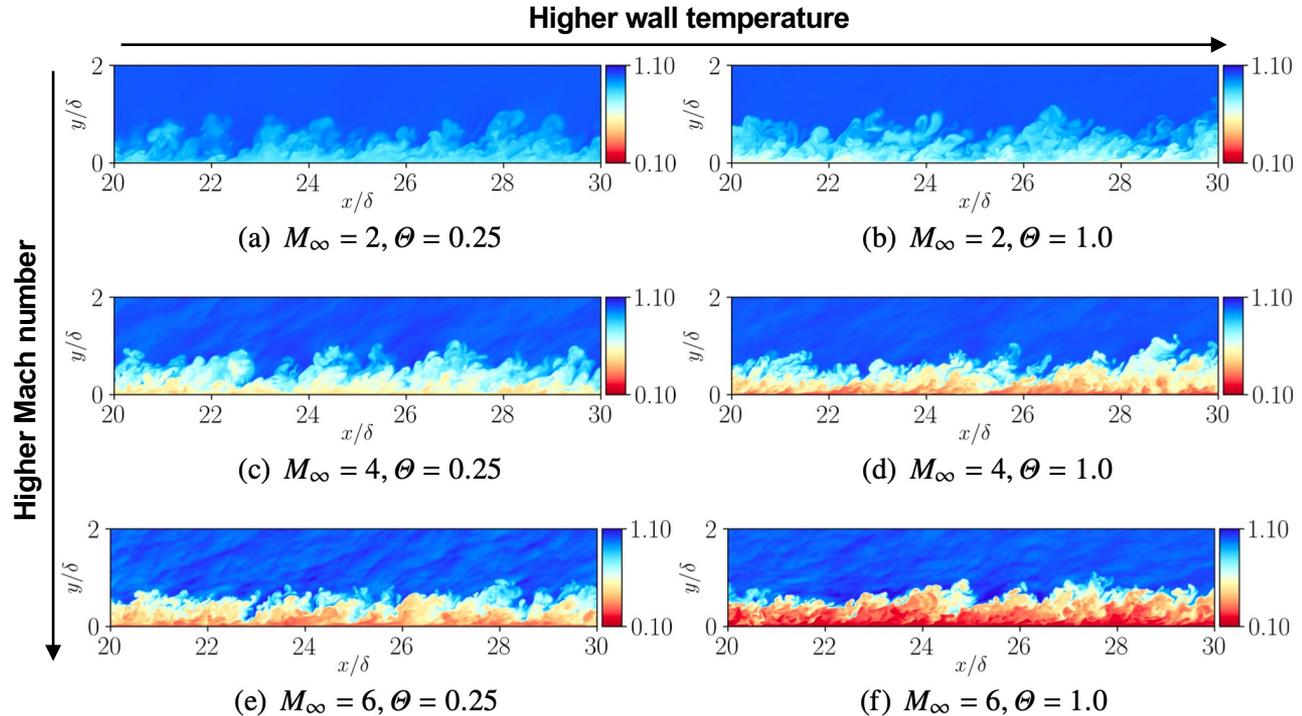
Effect of **Mach number** and **wall temperature** on high-speed zero-pressure-gradient turbulent boundary layers

Key points discussed:

- Correlation between velocity and temperature fluctuations
- Validity of the Reynolds analogy
- Modulation of scales separation
- Similarities and differences of Mach number and wall-cooling effects

Database:

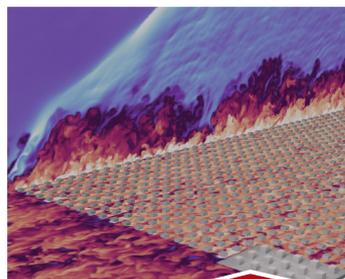
- $M_\infty = 2, 4, 6$
- $Re_\tau = 450$
- $\Theta = 0.25, 0.5, 0.75, 1$ (non-dimensional wall temperature)



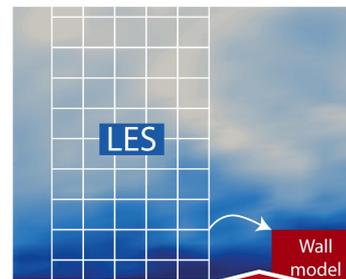
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Boundary layer with surface roughness:

Typically high-speed vehicles exhibit regular or irregular patterns of roughness.

Turbulent boundary layers exhibit higher skin friction and mixing, causing increased vehicle drag and heating.

Key questions:

- How does surface roughness affects turbulence near the wall at high speeds?
- What is the effect of Mach number and roughness level in the alteration of drag and heat transfer?



Space shuttle Discovery

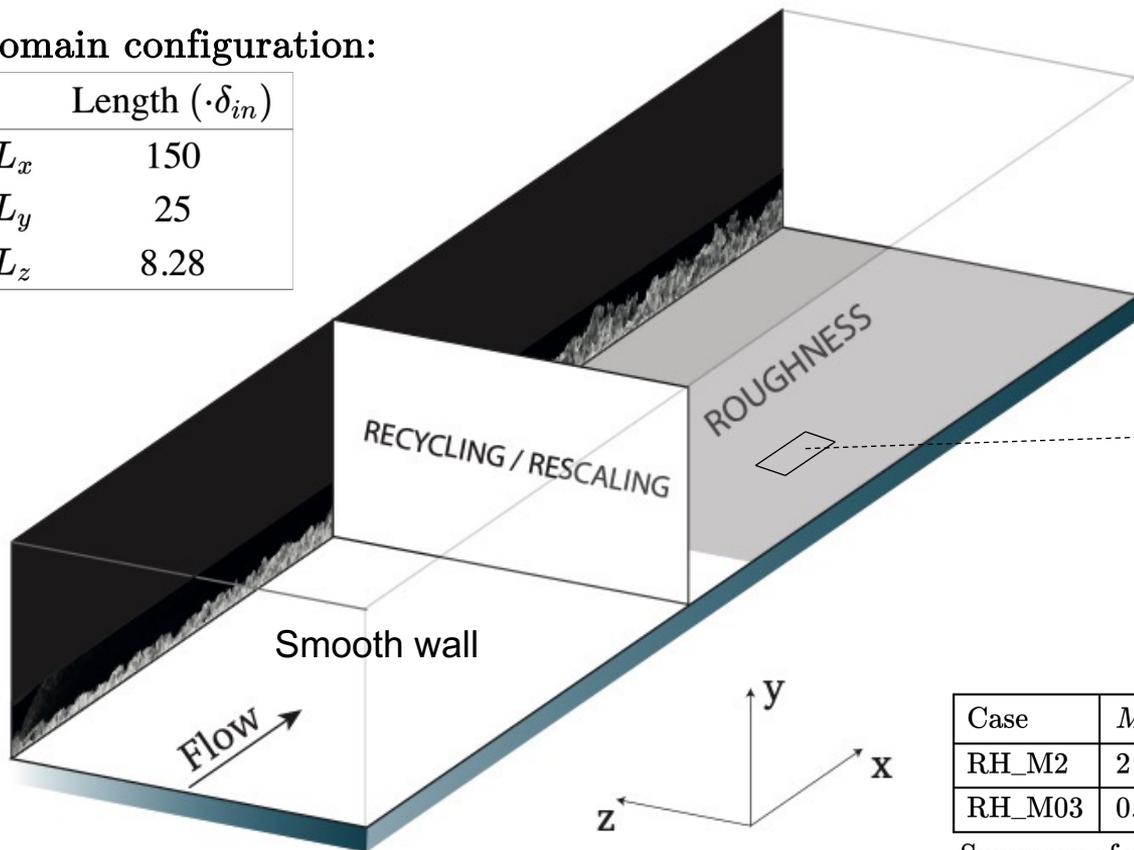


Apollo 12 heat shield

Task #2: Computational domain

Domain configuration:

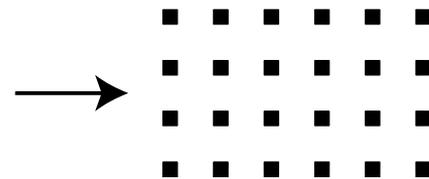
| | Length ($\cdot \delta_{in}$) |
|-------|--------------------------------|
| L_x | 150 |
| L_y | 25 |
| L_z | 8.28 |



Recycling station: $x = 40 \delta_{in}$

Roughness starts: $x = 55 \delta_{in}$

Pattern of aligned cubical elements:



$$\lambda_x = \lambda_z = 2k$$

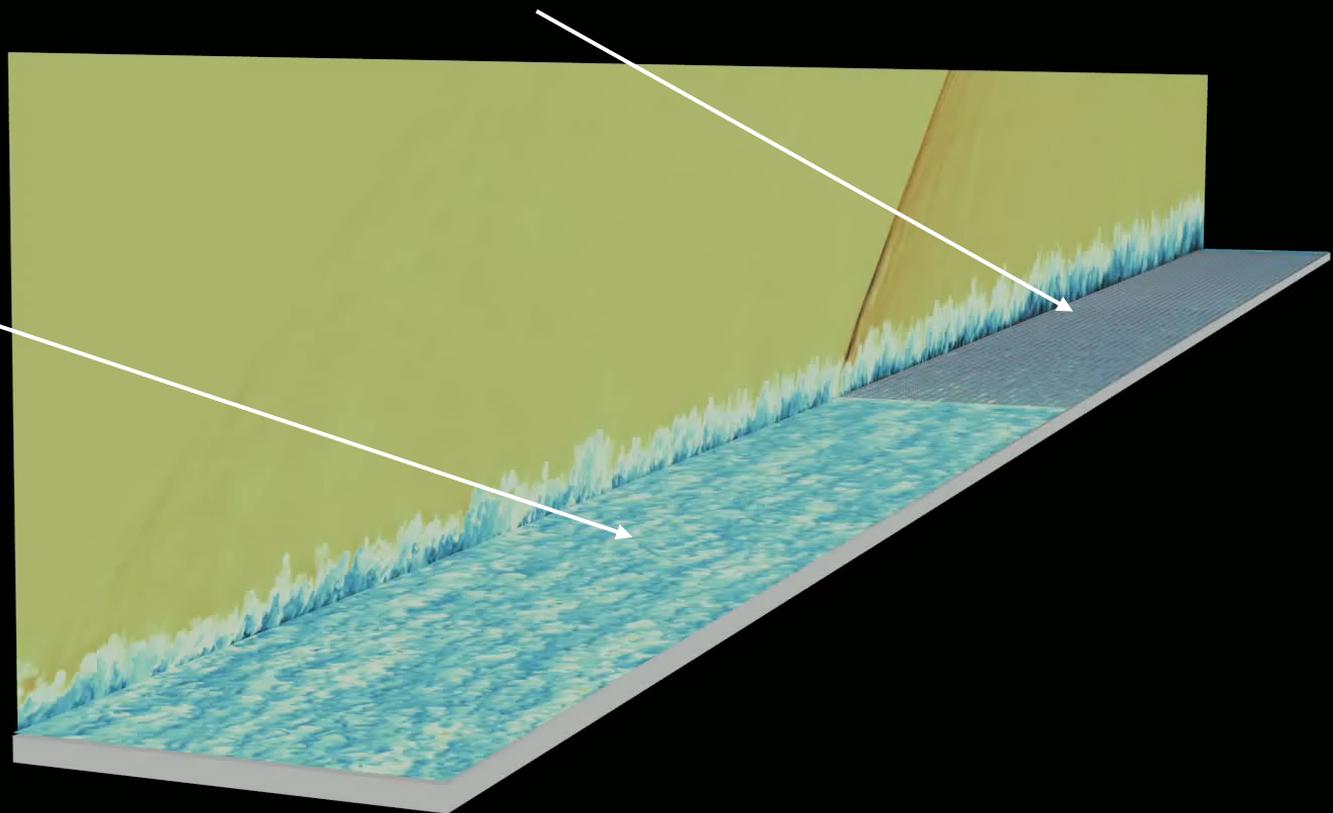
$$k = 0.12 \delta_{inflow}$$

| Case | M_∞ | Re_τ | N_x | N_y | N_z | $N_{nodes} \cdot 10^9$ |
|--------|------------|------------|-------|-------|-------|------------------------|
| RH_M2 | 2 | 600 – 1600 | 20240 | 556 | 1408 | 15.8 |
| RH_M03 | 0.3 | 650 – 1700 | 20240 | 556 | 1408 | 15.8 |

Summary of parameters of DNS study

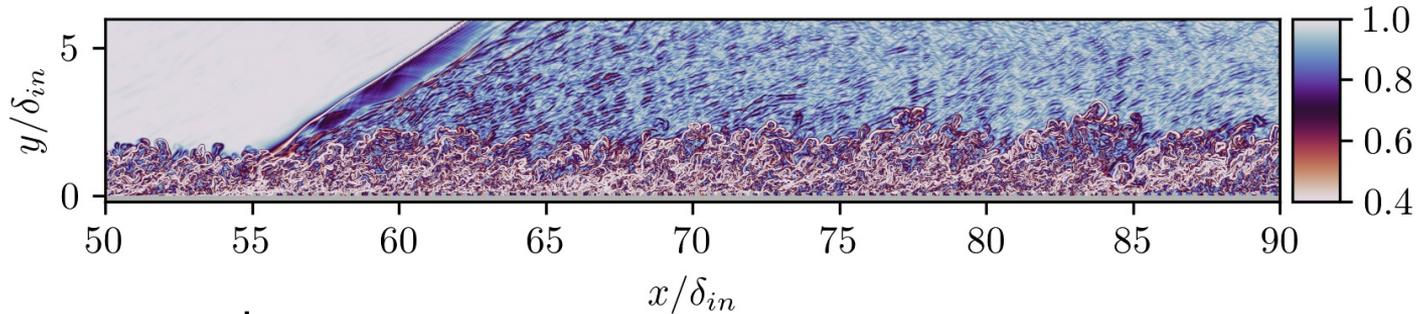
Smooth part

Rough part

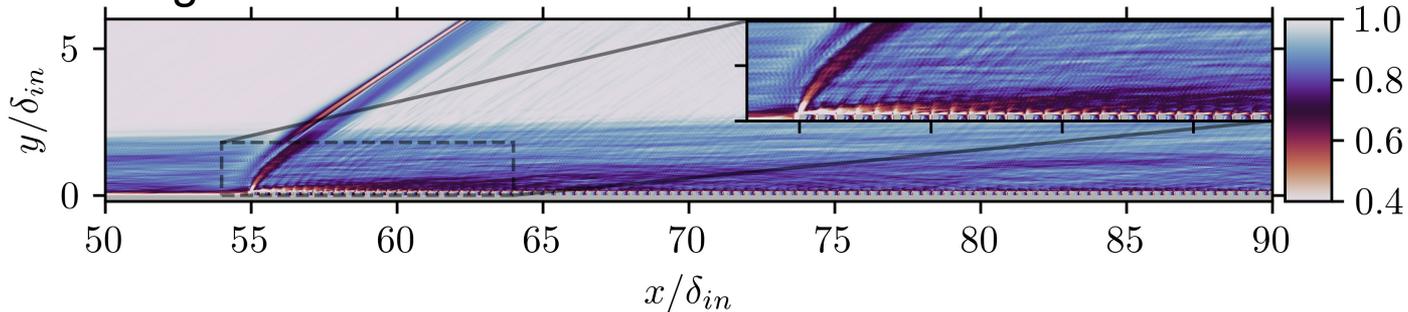


Wall-normal planes colored by the density gradient normalized between 0 and 1

RH_M2 instantaneous



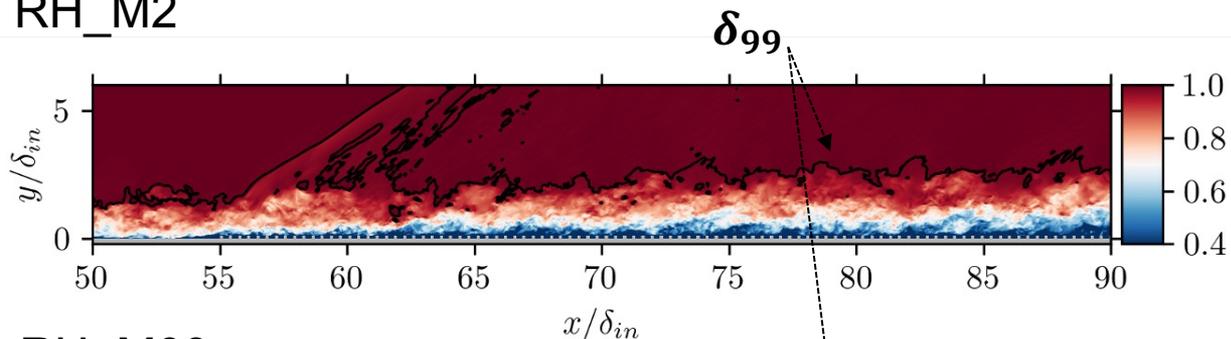
RH_M2 time averaged



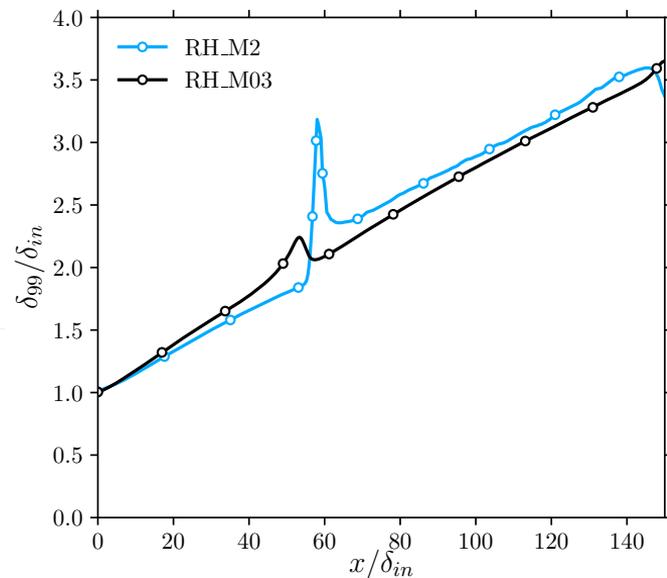
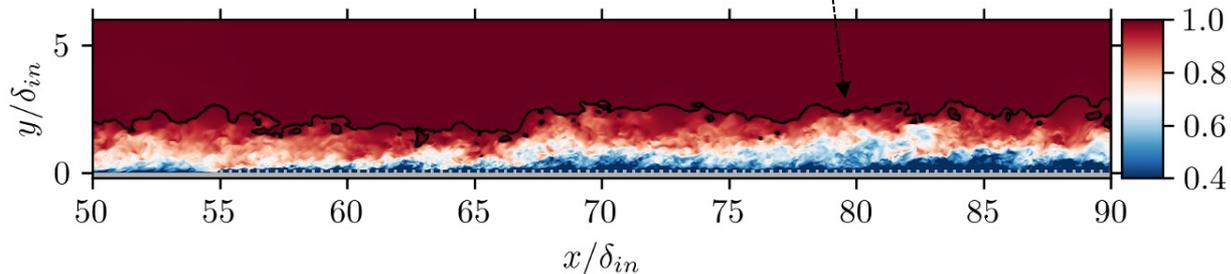
The supersonic case shows an initial shock wave that is followed by a pattern of compression/expansion waves emanated from each element

Wall-normal planes colored by streamwise velocity normalized between 0 and 1

RH_M2

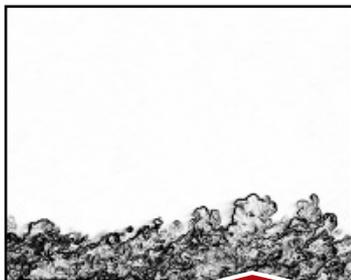


RH_M03

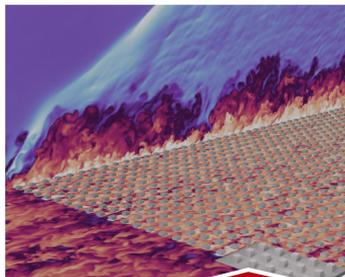


After the surface transition, the supersonic case has a more pronounced upward shift of the BL thickness. This fact contributes to the delay of equilibrium reached by the flow with the new surface.

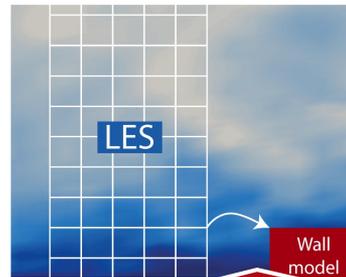
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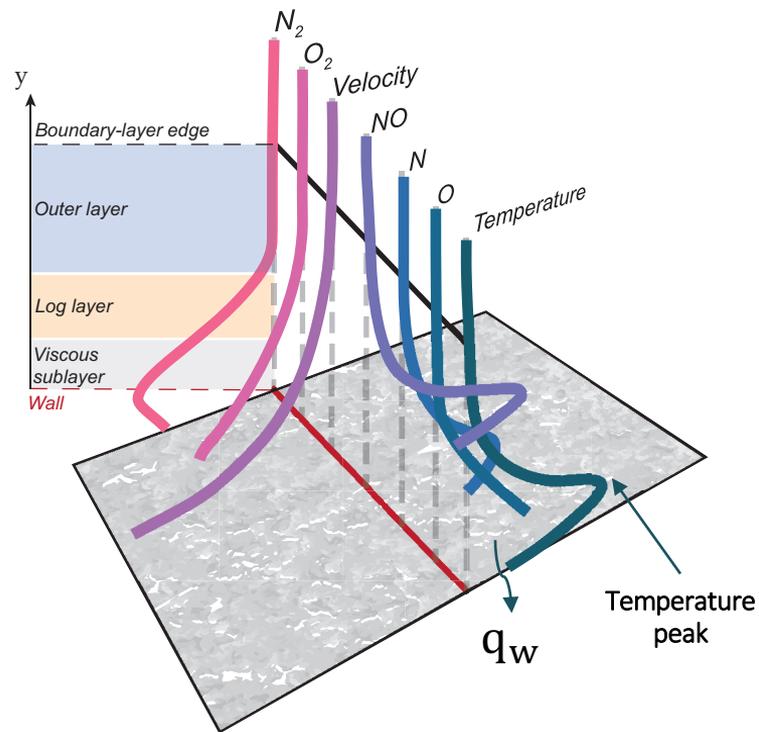
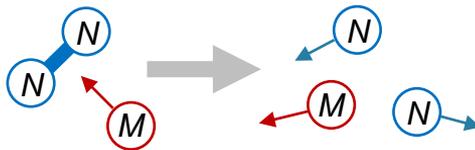
Task #3: Wall models for hypersonics

In high-speed boundary layers temperatures can get so high to activate chemical processes (dissociation and recombination of air).

At the present time, there are no wall-models able to predict the variation of composition in the boundary layer.

The objective of this work is to develop and test new wall-models in the form of ordinary differential equations that can instantaneously predict:

- Velocity u
- Temperature T
- Mass fractions (O_2, N_2, NO, O, N)





Hypersonic boundary layers

For this study, the DNS dataset of *Williams et al. (2023)** is considered:

$$Re_\tau = \frac{\delta}{l_v} \approx 1200, \quad M_\infty = 20, \quad Y_{O_2}^{wall} \approx 0.02, \quad T_w \approx 3000K$$

Friction Reynolds number

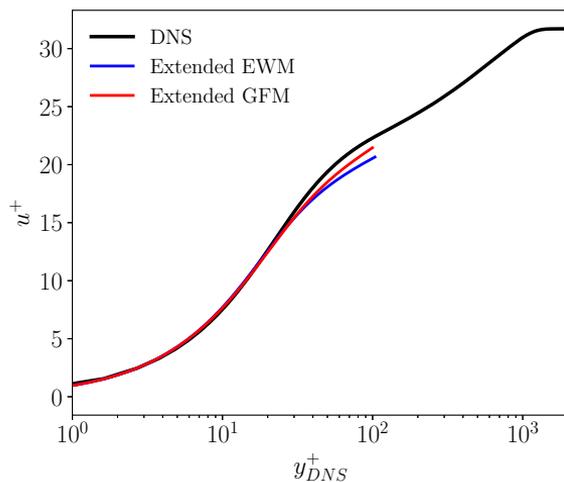
Edge Mach number

Mass fraction of O_2
at the wall

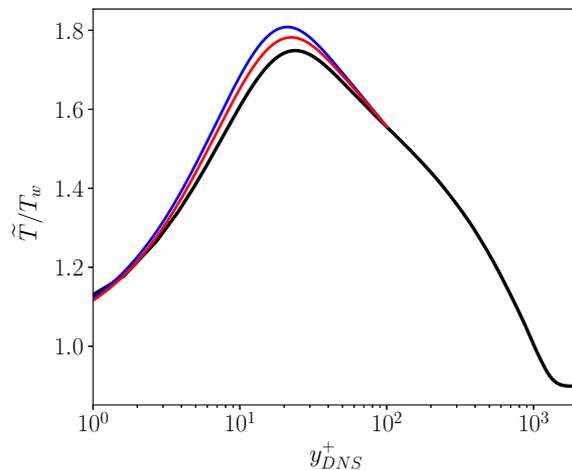
Wall temperature

- Benchmark DNS
- Previous model
- Proposed model

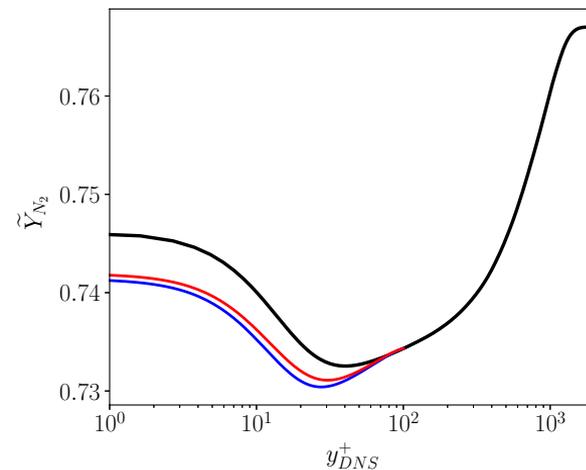
Velocity



Temperature



Molecular Nitrogen

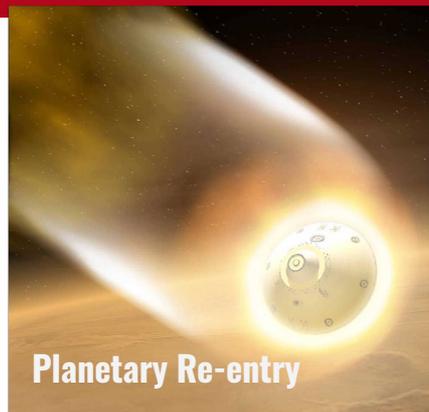


The proposed model shows improved results for velocity and temperature, further improvements are needed for the prediction of chemical composition

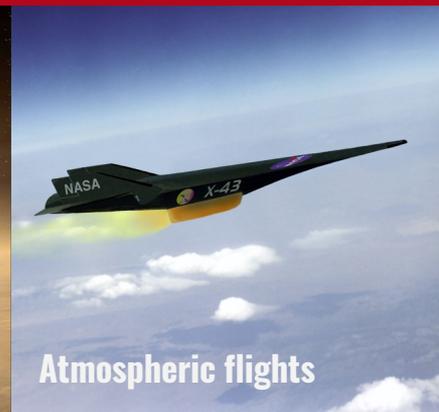
Summary of the past and future activities

- Investigation of the physics phenomena related to high-speed turbulent flows using high fidelity methodologies (DNS) on simple geometries.
- Application of high fidelity methodologies (DNS + IBM) on rough surfaces. Investigation of different geometries and Mach number effect.
- Development and testing of wall-models for high-speed boundary layers with chemical reactions.

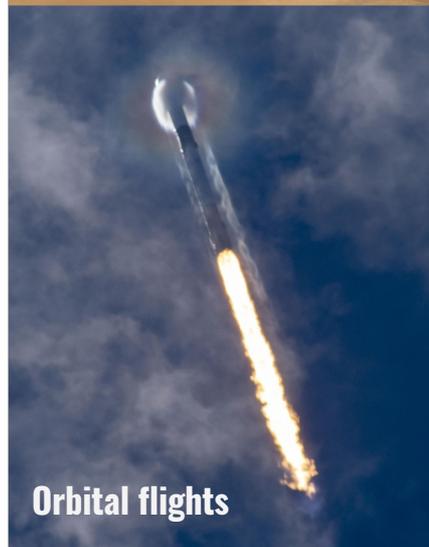
Several other applications are directly related to the research activity!



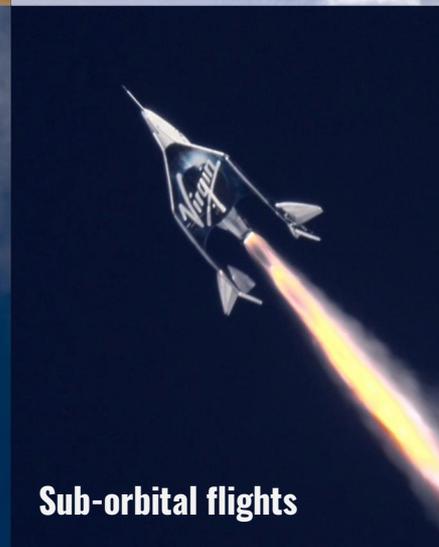
Planetary Re-entry



Atmospheric flights



Orbital flights



Sub-orbital flights

Publications:

- **Cogo, M.**, Salvatore, F., Picano, F., & Bernardini, M. (2022). *Direct numerical simulation of supersonic and hypersonic turbulent boundary layers at moderate-high Reynolds numbers and isothermal wall condition*. *Journal of Fluid Mechanics*
- De Vanna, F., Avanzi, F., **Cogo, M.**, Sandrin, S., Bettencourt, M., Picano, F., & Benini, E. (2023). *URANOS: A GPU accelerated Navier-Stokes solver for compressible wall-bounded flows*. *Computer Physics Communications*, 287, 108717.
- Placco, L., **Cogo, M.**, Bernardini, M., Aboudan, A., Ferri, F., & Picano, F. (2023). Large-Eddy Simulation of the unsteady supersonic flow around a Mars entry capsule at different angles of attack. *Aerospace Science and Technology*, 143, 108709.
- **Cogo, M.**, Baù, U., Chinappi, M., Bernardini, M., & Picano, F. (2023). Assessment of heat transfer and Mach number effects on high-speed turbulent boundary layers. *Journal of Fluid Mechanics*, 974, A10.
- **Cogo, M.**, Williams, C. T., Griffin, K. P., Picano, F., & Moin, P. (2023). Inverse-velocity transformation wall model for reacting turbulent hypersonic boundary layers. *Center for Turbulence Research Annual Research Briefs*.
- **Cogo, M.**, Modesti, D., Bernardini, M. & Picano, F. (2024). Surface roughness effects on supersonic turbulent boundary layers. *Journal of Fluid Mechanics*, Under Review.

Conferences:

- 33rd Parallel CFD International Conference in Alba, Italy (25-27 May 2022).
- 14th European Fluid Mechanics Conference in Athens, Greece (13-16 September 2022).
- 76th Annual Meeting of the APS Division of Fluid Dynamics, Washington D.C. (19-21 November 2023)
- Invited talk at SISSA, Analysis Junior Seminar, SISSA Trieste, 16 February 2024
- Direct and Large-Eddy Simulation 14, Erlangen Germany, 10-12 April 2024
- PhD Days 2024, Scopello Italy, 6-9 May 2024

Visiting periods:

- Research period at TU Delft (Netherlands) hosted by prof. Davide Modesti (4 months)
- Research period at Stanford University (USA) hosted by prof. Parviz Moin (6 months). Supported by Fulbright scholarship and Zegna founder's scholarship.

Thanks for the attention



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