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Multiphysics modelling of thermal cracks in multiphase heterogenous porous materials

PhD Candidate: Zechao Chen -- 38th

Admission to the first year - 09/11/2022

Supervisor: Prof. Lorenzo Sanavia

Co-supervisor: Prof. Laura De Lorenzis, ETH Zurich

PhD Course in Sciences, Technologies And Measurements For Space

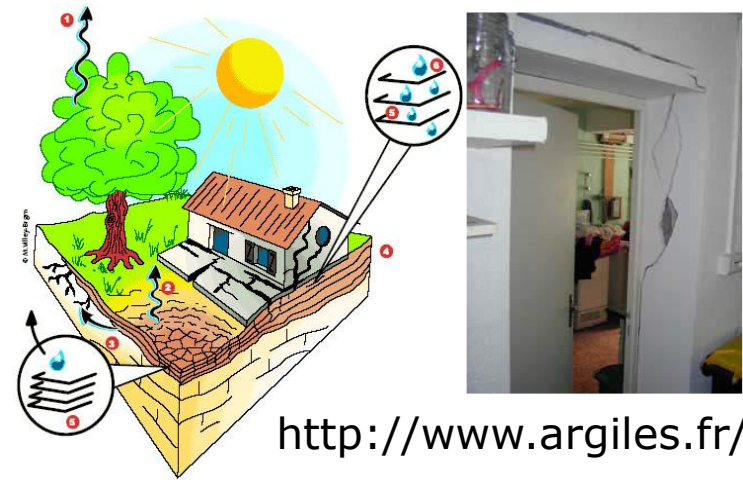
- 1. Introduction**
- 2. Research background**
- 3. Project objectives**
- 4. Work methodology**
- 5. Work schedule**

Motivation: cracks due to hydro-thermal effects

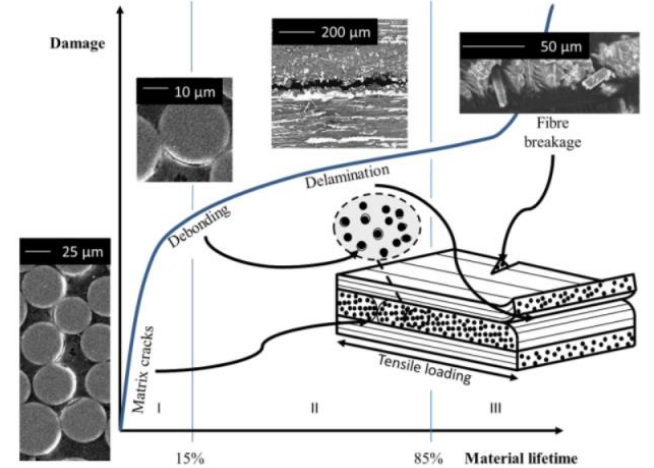


Geoenvironmental engineering

Desiccation (Laloui 2009)

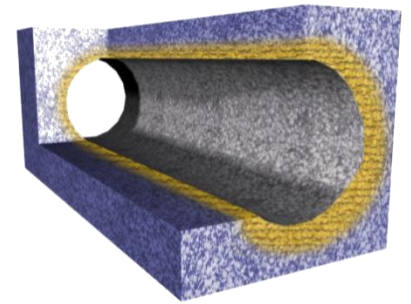


<http://www.argiles.fr/>

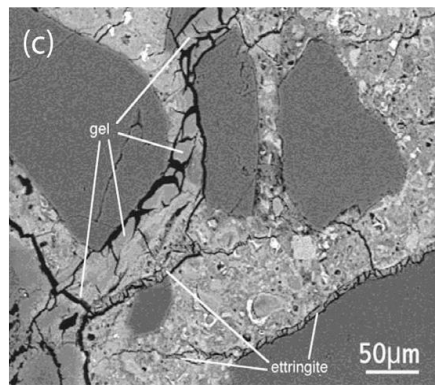


Damage in composite laminates
doi.org/10.1007/s10853-018-2045-6

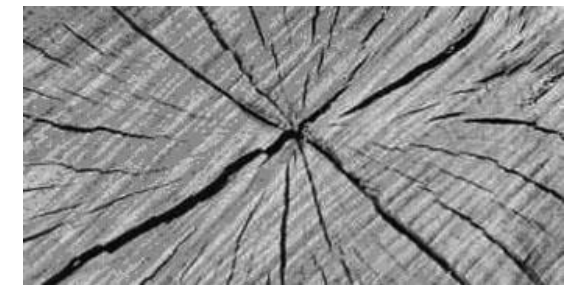
Desaturation/cracks
development of EDZ
(Excavation Damaged
Zone)



Deep nuclear waste
disposals



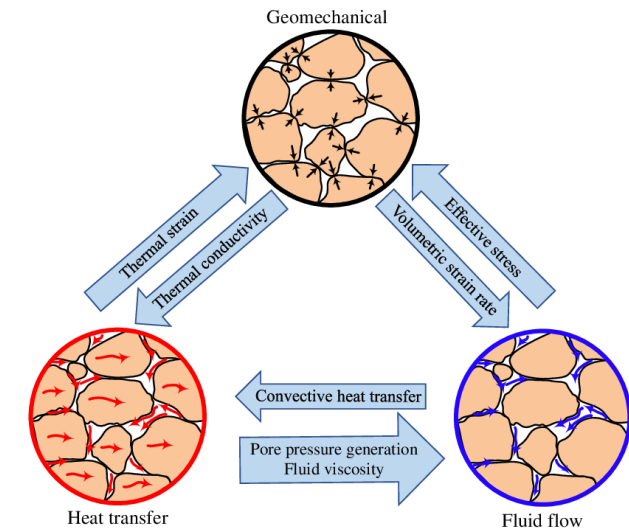
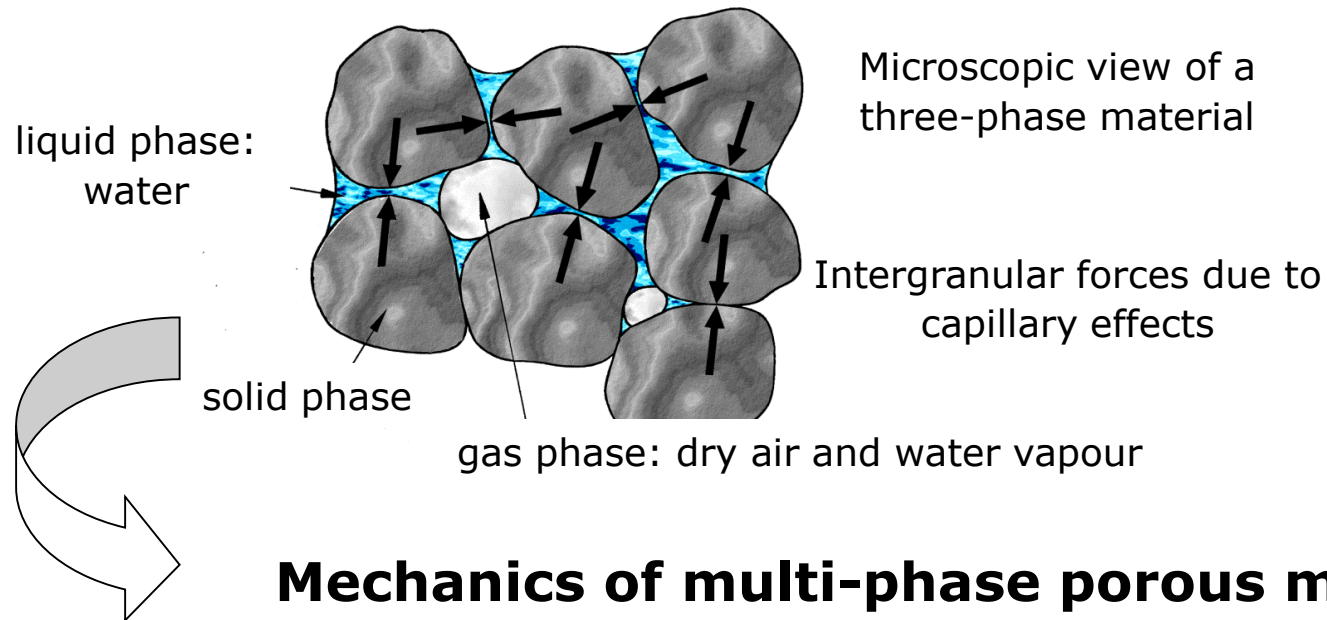
ASR (Alkali-Silica Reaction) shrinkage-
induced cracking in concrete



Cracks in wood

Multi-phase porous material

Composed by a solid skeleton with open pores containing one or more fluids



solid-fluids interaction, liquid-gas interaction, non-isothermal conditions

- Lewis, R. W., Schrefler, B. A. 1998. *The Finite Element Method in the Static and Dynamic Deformation and Consolidation of Porous Media (Second.)*. Chichester, UK: John Wiley & Sons.
- William G. Gray, Cass T. Miller 2014. *Introduction to the Thermodynamically Constrained Averaging Theory for Porous Medium Systems*. Springer.

Multi-phase porous material

Equilibrium equations (mixture; quasi-statics):

$$\operatorname{div}\left(\boldsymbol{\sigma}' - \left[p^g - S_w p^c\right] \mathbf{1}\right) + \rho \mathbf{g} = 0$$

Mass balance equation (solid, liquid water and water vapour):

$$\begin{aligned} & n \left[\rho^w - \rho^{gw} \right] \left[\frac{\partial S_w}{\partial t} \right] + \left[\rho^w S_w - \rho^{gw} [1 - S_w] \right] \operatorname{div} \left(\frac{\partial \mathbf{u}}{\partial t} \right) + [1 - S_w] n \left[\frac{\partial \rho^{gw}}{\partial t} \right] \\ & - \operatorname{div} \left(\rho^g \frac{M_a M_w}{M_g^2} \mathbf{D}_g^{gw} \operatorname{grad} \left(\frac{\partial p^{gw}}{\partial p^g} \right) \right) + \operatorname{div} \left(\rho^w \frac{\mathbf{k} \mathbf{k}^{rw}}{\mu^w} \left[-\operatorname{grad}(p^g) + \operatorname{grad}(p^c) + \rho^w \mathbf{g} \right] \right) \\ & + \operatorname{div} \left(\rho^{gw} \frac{\mathbf{k} \mathbf{k}^{rg}}{\mu^g} \left[-\operatorname{grad}(p^g) + \rho^g \mathbf{g} \right] \right) - \beta_{swg} \frac{\partial T}{\partial t} = 0 \end{aligned}$$

- Lewis, R. W., Schrefler, B. A. 1998. *The Finite Element Method in the Static and Dynamic Deformation and Consolidation of Porous Media (Second.)*. Chichester, UK: John Wiley & Sons.

Multi-phase porous material

Dry air mass balance equation:

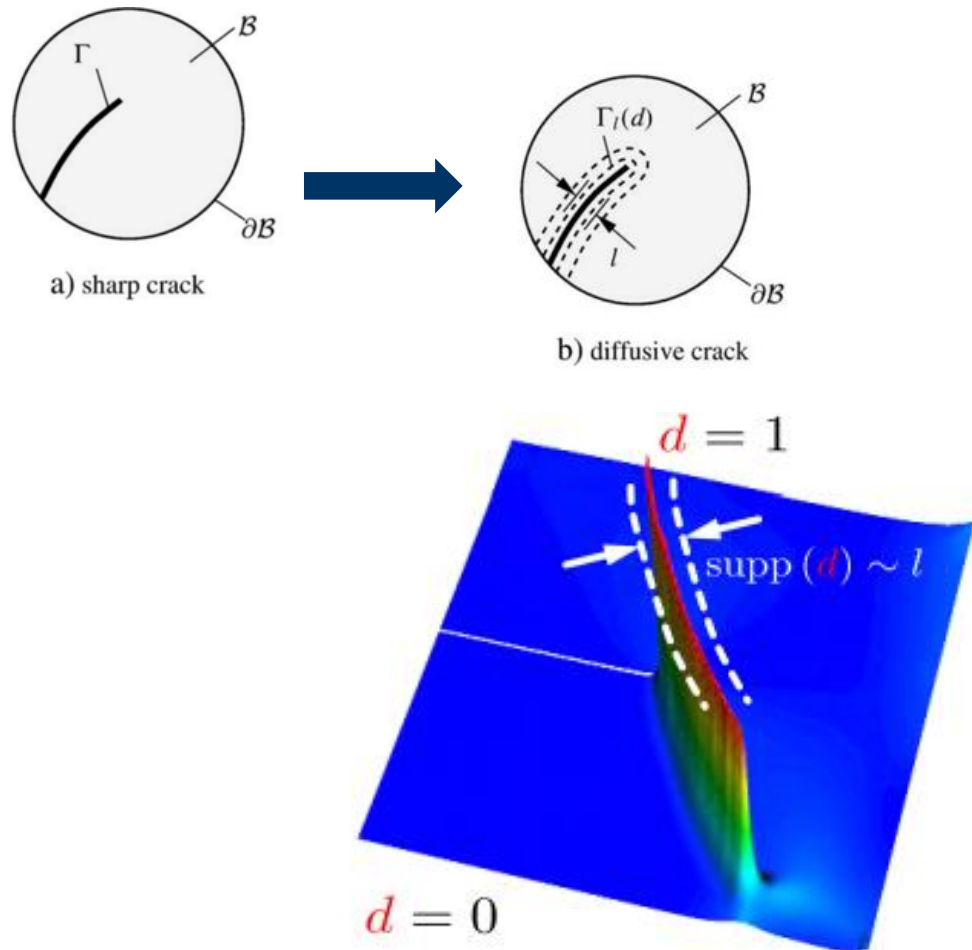
$$\begin{aligned}
 & -n\rho^{ga} \left[\frac{\partial S_w}{\partial t} \right] + \rho^{ga} [1 - S_w] \operatorname{div} \left(\frac{\partial \mathbf{u}}{\partial t} \right) + nS_g \frac{\partial \rho^{ga}}{\partial t} - \operatorname{div} \left(\rho^g \frac{M_a M_w}{M_g^2} \mathbf{D}_g^{ga} \operatorname{grad} \left(\frac{p^{ga}}{p^g} \right) \right) \\
 & + \operatorname{div} \left(\rho^{ga} \frac{\mathbf{k}k^{rg}}{\mu^g} \left[-\operatorname{grad}(p^g) + \rho^g \mathbf{g} \right] \right) - [1 - n] \beta_{swg} \rho^{ga} [1 - S_w] \frac{\partial T}{\partial t} = 0
 \end{aligned}$$

Energy balance equation (mixture):

$$\begin{aligned}
 & \left(\rho C_p \right)_{\text{eff}} \frac{\partial T}{\partial t} + \rho^w C_p^w \left(\frac{\mathbf{k}k^{rw}}{\mu^w} \left[-\operatorname{grad}(p^g) + \operatorname{grad}(p^c) + \rho^w \mathbf{g} \right] \right) \cdot \operatorname{grad}(T) \\
 & + \rho^g C_p^g \left(\frac{\mathbf{k}k^{rg}}{\mu^g} \left[-\operatorname{grad}(p^g) + \rho^g \mathbf{g} \right] \right) \cdot \operatorname{grad}(T) - \operatorname{div} \left(\chi_{\text{eff}} \operatorname{grad}(T) \right) = -\dot{m}_{\text{vap}} \Delta H_{\text{vap}}
 \end{aligned}$$

- Lewis, R. W., Schrefler, B. A. 1998. *The Finite Element Method in the Static and Dynamic Deformation and Consolidation of Porous Media (Second.)*. Chichester, UK: John Wiley & Sons.

The Phase-Field Method (PFM) to fracture



Key advantages

- Flexibility (initiation, propagation, merging, branching)
- Variational framework
- Simple implementation

Disadvantages

- Fine mesh needed
- Efficiency/robustness of solution

• [SwissMech Seminars Archive – SwissMech Seminars](#)

The Phase-Field Method (PFM) to fracture

Sharp crack: (variational reformulation of) Griffith

$$\min_{\mathbf{u} \in \mathcal{U}_n(\Gamma_c), \Gamma_c \ni \Gamma_{cn-1}} \mathcal{E}(\mathbf{u}, \Gamma_c) = \underbrace{\int_{\Omega \setminus \Gamma_c} \psi(\varepsilon(\mathbf{u})) d\Omega}_{\text{elastic strain energy}} + \underbrace{G_c \mathbb{H}^{d-1}(\Gamma_c)}_{\text{fracture energy}} - \int_{\Omega} \mathbf{b}_n \cdot \mathbf{u} d\Omega - \int_{\partial\Omega_N} \mathbf{t}_n \cdot \mathbf{u} dS$$

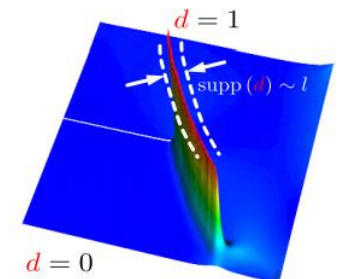
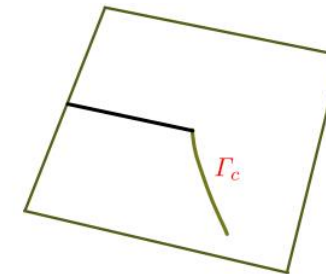
Francfort and Marigo (1998)
Mumford and Shah (1989)



regularization



$\ell \rightarrow 0$
 Γ -convergence



Diffusive crack: phase-field approach

$$\min_{\mathbf{u} \in \mathcal{U}_n, d \geq d_{n-1}} \mathcal{E}_\ell(\mathbf{u}, d) = \underbrace{\int_{\Omega} g(d) \psi(\varepsilon(\mathbf{u})) d\Omega}_{\text{elastic strain energy}} + \underbrace{\frac{G_c}{c_w} \int_{\Omega} \left[\frac{w(d)}{\ell} + \ell |\nabla d|^2 \right] d\Omega}_{\text{fracture energy}} - \int_{\Omega} \mathbf{b}_n \cdot \mathbf{u} d\Omega - \int_{\partial\Omega_N} \mathbf{t}_n \cdot \mathbf{u} dS$$

Bourdin et al. (2000)
Ambrosio and Tortorelli (2000)
Braides (1998)

The Phase-Field Method (PFM) to fracture

...with energy decomposition

$$\min_{\mathbf{u} \in \mathcal{U}_n, d \geq d_{n-1}} \mathcal{E}_\ell(\mathbf{u}, d) = \int_{\Omega} [g(d)\psi^+(\varepsilon(\mathbf{u})) + \psi^-(\varepsilon(\mathbf{u}))] d\Omega + \frac{G_c}{c_w} \int_{\Omega} \left[\frac{w(d)}{\ell} + \ell |\nabla d|^2 \right] d\Omega - \int_{\Omega} \mathbf{b}_n \cdot \mathbf{u} d\Omega - \int_{\partial\Omega_N} \mathbf{t}_n \cdot \mathbf{u} dS$$

Amor et al. (2009)

Miehe et al. (2010) Freddi and Royer-Carfagni (2010)

Phase-field evolution equation $-2l\Delta d + \frac{1}{2l}d = \frac{2(1-d)}{G_c} \mathcal{H} \quad \mathcal{H}(\mathbf{x}, t) := \max_{\tau \in [0, t]} \Psi^+(\varepsilon(\mathbf{x}, \tau))$

$g(d)$: degradation function

ψ : energy storage function (ψ^+ refers to tension and ψ^- is compression)

G_c : fracture toughness

$w(d)$: local damage function

ℓ : crack length scale parameter

∇d : spatial gradient

\mathbf{u} : displacement field

c_w : normalization constant

d : fracture phase field

\mathbf{b}_n : body force vector \mathbf{t}_n : face force vector

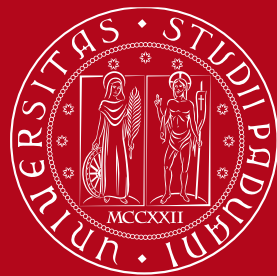
• [SwissMech Seminars Archive – SwissMech Seminars](#)

Develop a THM (Thermo-Hydro-Mechanical) crack Phase-field numerical model

- Develop a numerical model able to study the nucleation and propagation of cracks induced by **thermal effects** in multiphase heterogenous porous materials.
- Merge a **thermodynamically consistent multiphase porous media model** (and the associated finite element code Comes-Geo developed at the UNIPD) with a **crack phase-field model** (and the associated FEM code for brittle fracture developed at ETH Zurich).
- After **validation with experiments** designed from the numerical modelling, the model will be further **extended**.
- Application to study cracks in clayey materials and in heterogeneous composite materials.

Thanks for the attention

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