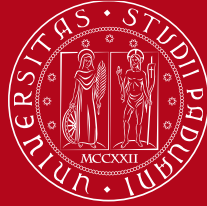


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Peridynamic modelling of crack propagation in inelastic materials for aerospace applications

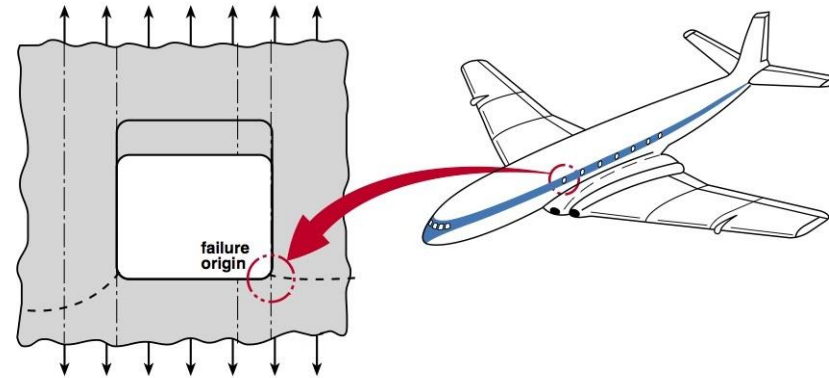
Atefeh Pirzadeh - 36th Cycle

Supervisor: Prof. Ugo Galvanetto

Co-supervisors: Prof. Mirco Zaccariotto, Dr. Federico Dalla Barba

Meeting - 09 November

- The most used commercial aerospace structural materials are aluminum alloys, titanium alloys, high-strength steels, and composites.
- Aerospace structures are subjected to different kinds of load, which may cause them to experience failure in some parts.
- Analysis of crack propagation in solid materials is very relevant to practical applications.



Classical theory of continuum mechanics

Some limitations for studying crack propagation

- It has partial derivatives with respect to spatial coordinates, which are undefined along the cracks
- To compensate this weakness, the problem is redefined along the cracks
- Not appropriate for spontaneous cracks
- Some assumptions like the time crack initiates and crack growth speed

Simulating crack propagation is a challenging task

Finite Element Method (FEM), Extended FEM (XFEM) and Meshless Methods

Peridynamic is a nonlocal continuum mechanics theory (developed by Silling in 2000).

- Modeling problems with singularities like cracks
- Appropriate for large number of cracks
- Integration is used instead of differentiation

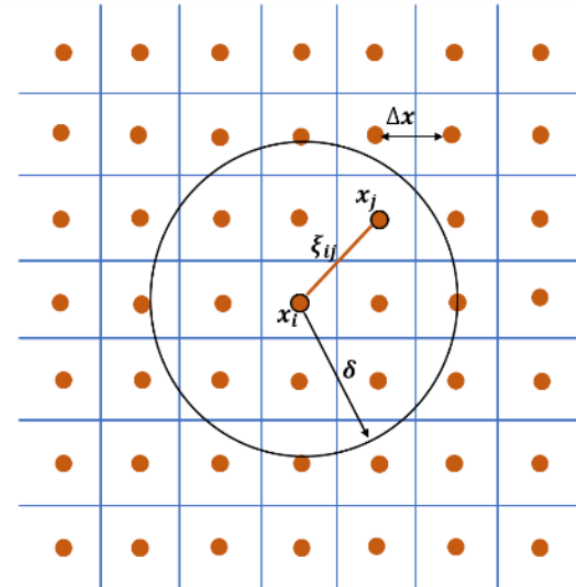
$$\rho(\mathbf{x}_i) \ddot{\mathbf{u}}_{n+1}(\mathbf{x}_i) = \sum_j (\underline{\mathbf{T}}_n[\mathbf{x}_i](\mathbf{x}_j - \mathbf{x}_i) - \underline{\mathbf{T}}_n[\mathbf{x}_j](\mathbf{x}_i - \mathbf{x}_j)) \Delta V \mathbf{x}_{ij} + \mathbf{b}_n(\mathbf{x}_i)$$

Bond-based

- The force in each bond does not depend on other bonds deformation
- Can not enforce incompressible shear deformation

Ordinary-State-based

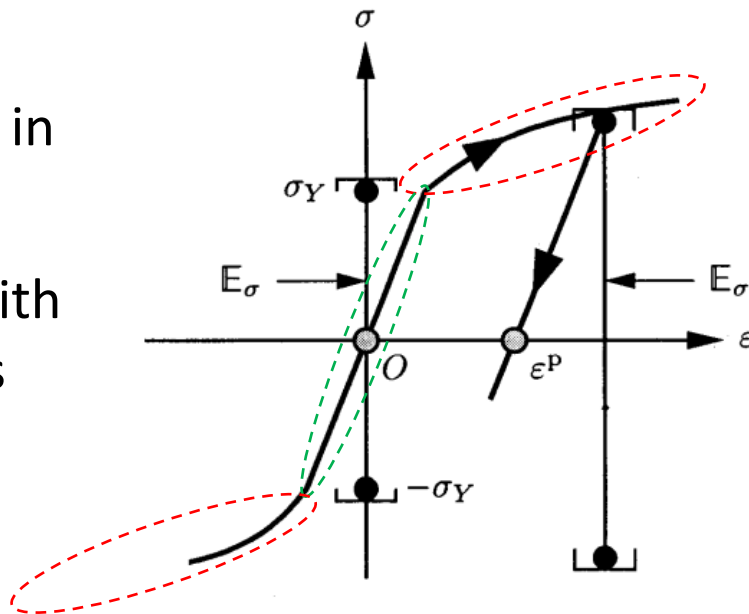
- The force of each bond depends on all the bonds inside the horizon



Most of the Peridynamic based models are used for fracture analysis in **Elastic Domain**.

Before crack initiation, most materials experience deformation in **Plastic Domain**.

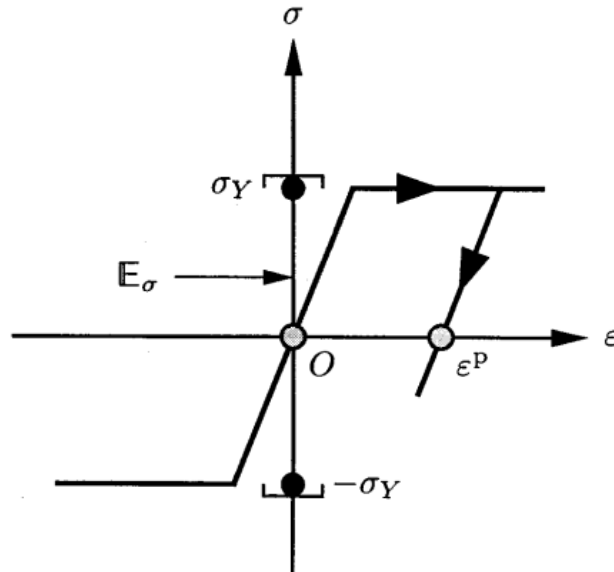
Equipping the bonds of **OSB-PD** with an **Elastoplastic** constitutive law is the objective of this research.



Motivation for Elastoplastic Approach

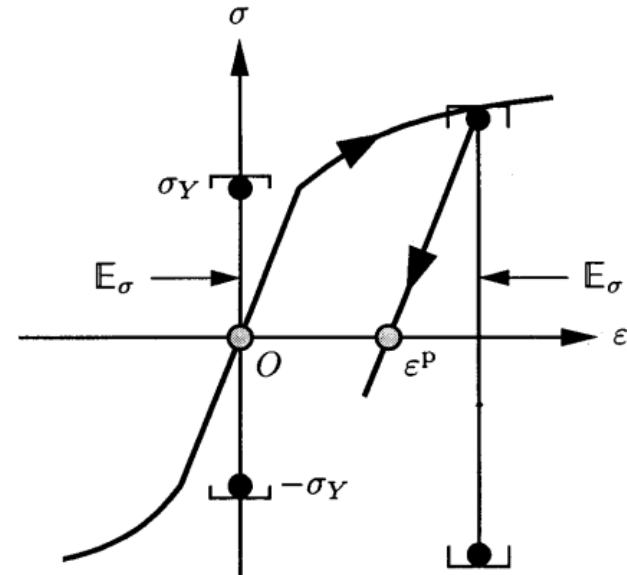
Materials with **perfect plasticity**:

Closure of the elastic range (E_σ) remains unchanged.



Materials with **strain hardening**:

Closure of the elastic range (E_σ) expands with the amount of slip in plastic domain.



Kuhn-Tucker condition:

$$\lambda f(\sigma, \alpha, q) = 0, \quad \lambda = |\dot{\varepsilon}_p|$$



Consistency condition:

$$\lambda \dot{f}(\sigma, \alpha, q) = 0$$

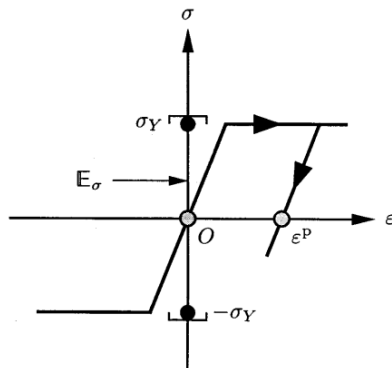
Elastic stress-strain
relationship:

$$\sigma = E(\varepsilon - \varepsilon_p)$$

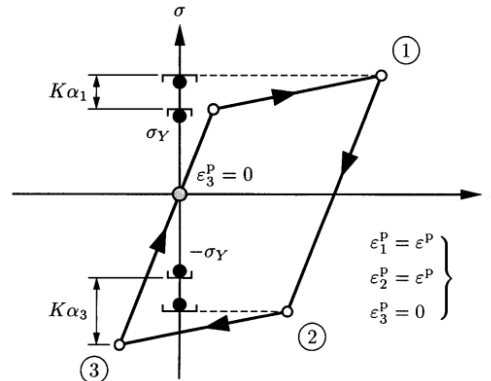
Yield condition:

$$f(\sigma, \alpha, q) = |\sigma - q| - (\sigma_Y + K\alpha) \leq 0$$

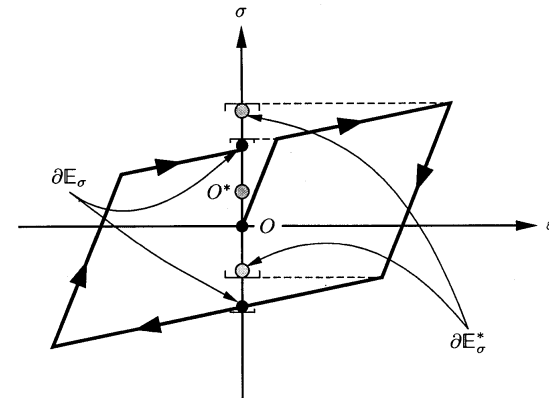
$$\left\{ \begin{array}{l} \dot{\alpha} = \dot{\varepsilon}^p \operatorname{sign}(\sigma - q) \quad \text{Isotropic hardening} \\ \dot{q} = \dot{\varepsilon}^p H \quad \text{Kinematic hardening} \end{array} \right.$$



Perfect plasticity



Isotropic hardening



Kinematic hardening

In J2 plasticity, the von-Mises yield criterion is used based on maximum deviatoric strain energy. for 3D case:

$$f(\underline{t}_{trial}^d) = \frac{\|\underline{t}_{trial}^d\|^2}{2} - \psi_0 \equiv f(\sigma, \alpha, q) = |\sigma - q| - (\sigma_Y + K\alpha) \leq 0$$

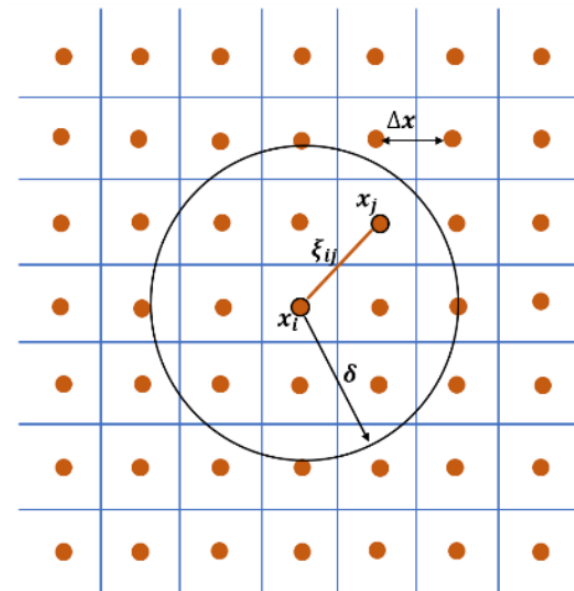
Yield condition:

$$\text{if } f(\underline{t}_{trial}^d) \leq 0 \Rightarrow \text{elastic step } (\Delta\lambda = 0) \Rightarrow \begin{cases} \underline{t}_n^d = \underline{t}_{trial}^d \\ \underline{e}_n = \underline{e}_{trial} \end{cases}$$

$$\text{if } f(\underline{t}_{trial}^d) > 0 \Rightarrow \text{plastic step } (\Delta\lambda \neq 0) \Rightarrow \begin{cases} f(\underline{t}^d) = 0 & \text{Yield condition} \\ \lambda \dot{f}(\underline{t}^d) = 0 & \text{Consistency condition} \end{cases}$$

$$\underline{e}_n^{dp} = \underline{e}_{n-1}^{dp} + \Delta\lambda \underline{t}_n^d$$

Dynamic relaxation method is used to calculate next step trial bond extension and bond force.

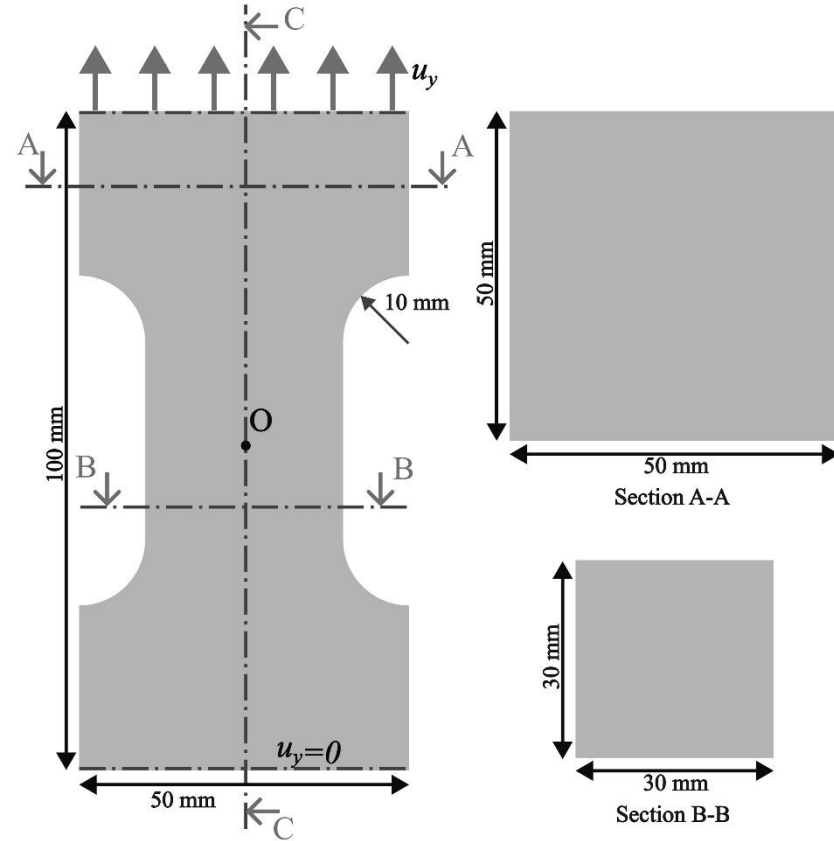
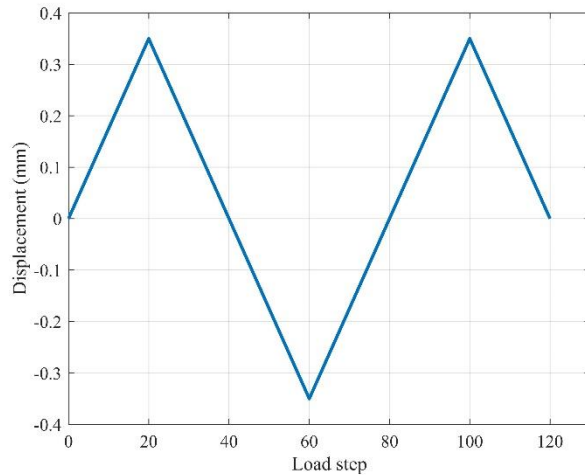


$$E=200 \text{ GPa} \quad \nu=0.3$$

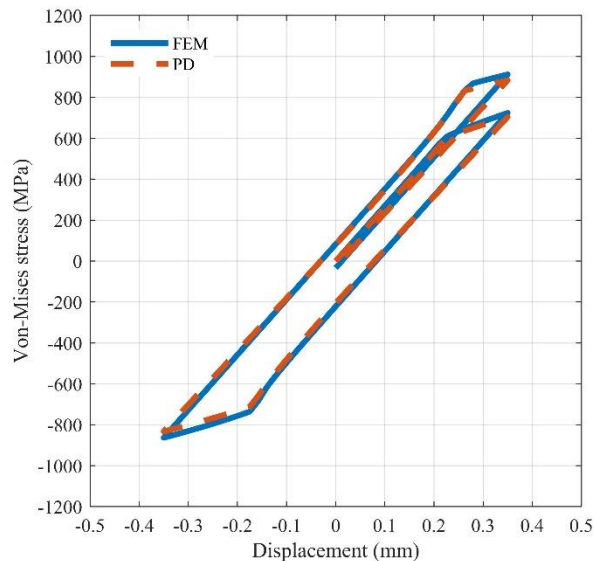
$$\rho=8000 \text{ kg/m}^3$$

$$\sigma_y=600 \text{ MPa}$$

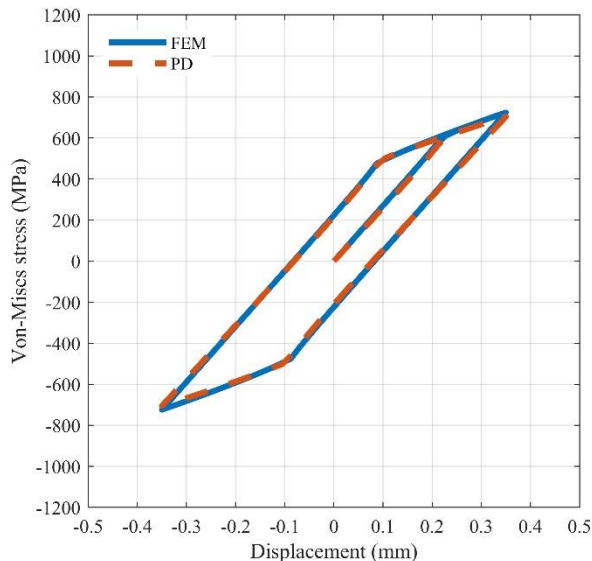
$$K=20 \text{ GPa} \quad H=20 \text{ GPa}$$



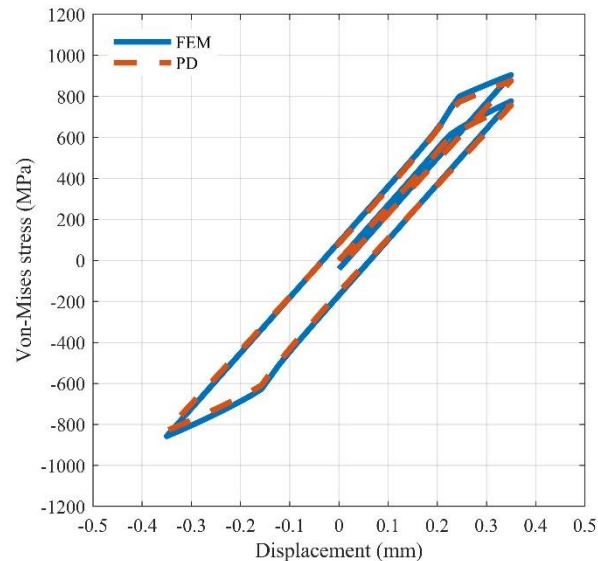
Stress at central node (Node O):



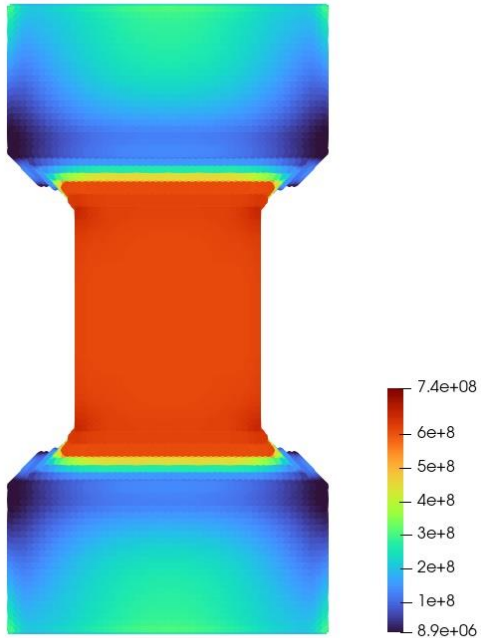
Isotropic hardening



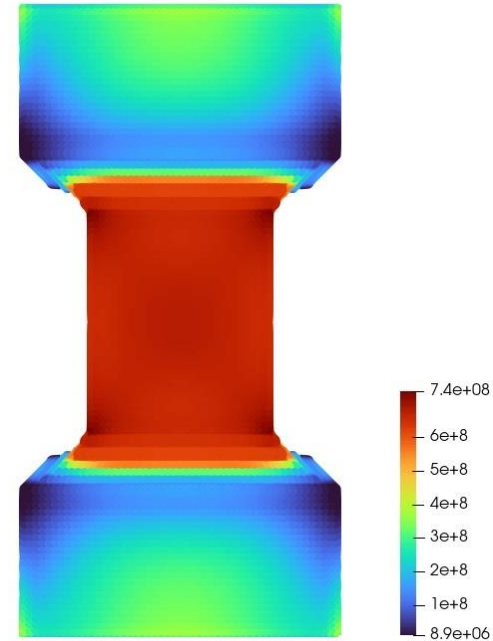
Kinematic hardening



Mixed hardening



Von-mises stress when $u_y = 0.21$ mm



Von-mises stress when $u_y = 0.35$ mm

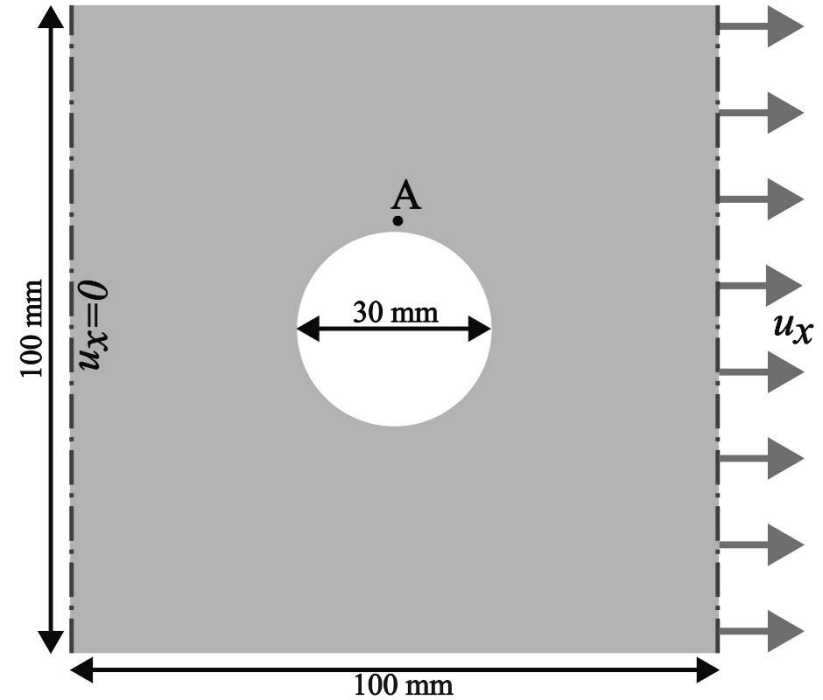
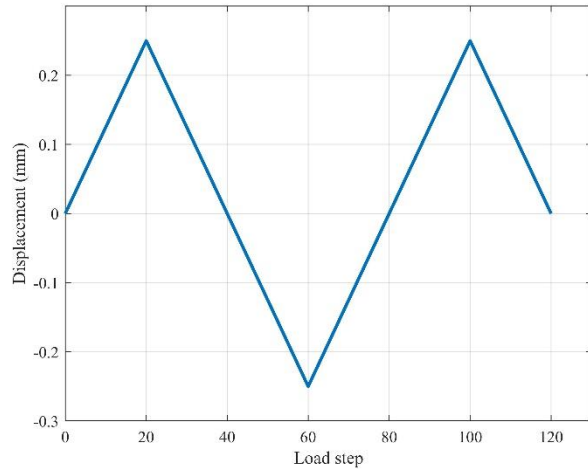
2D square plane stress example

$$E=200 \text{ GPa} \quad \nu=0.3$$

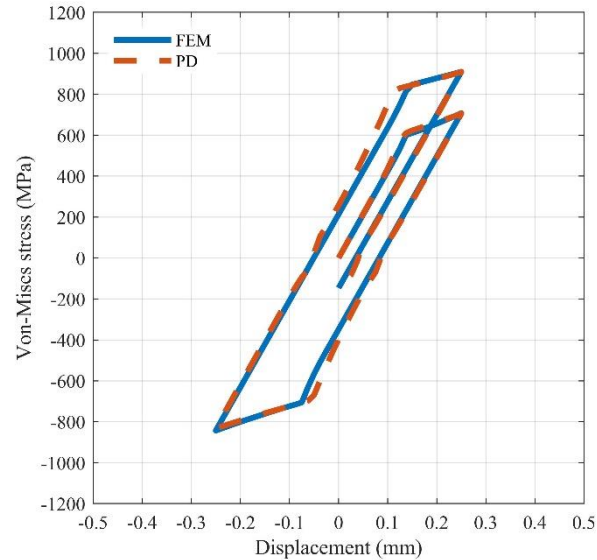
$$\rho=8000 \text{ kg/m}^3$$

$$\sigma_y=600 \text{ MPa}$$

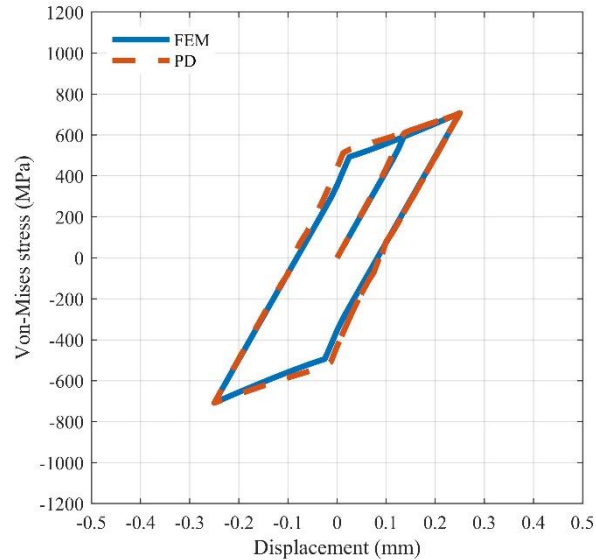
$$K=20 \text{ GPa} \quad H=20 \text{ GPa}$$



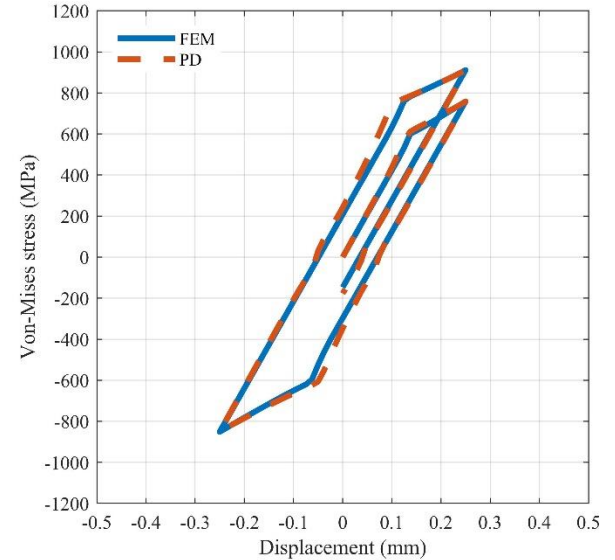
Stress at node A:



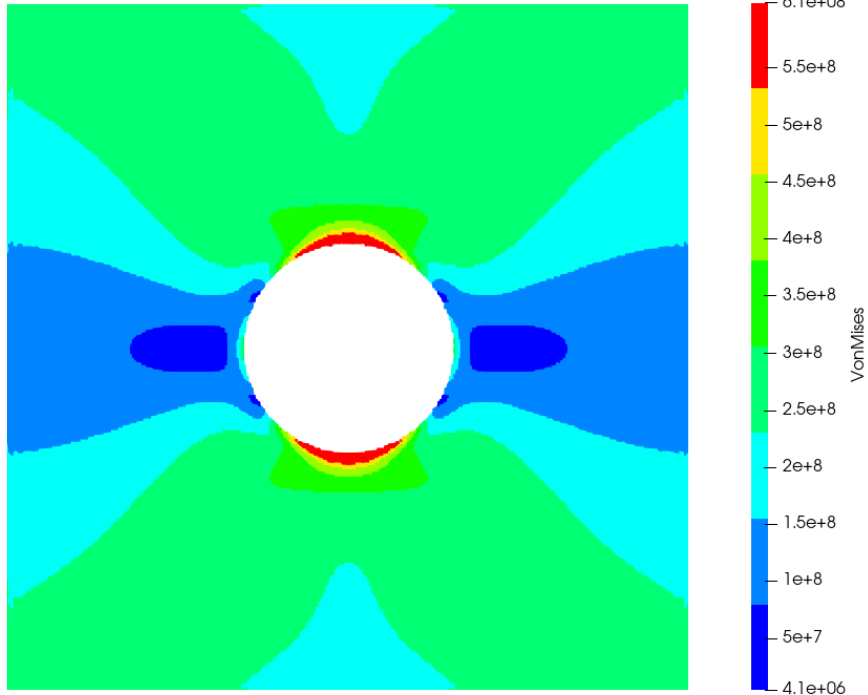
Isotropic hardening



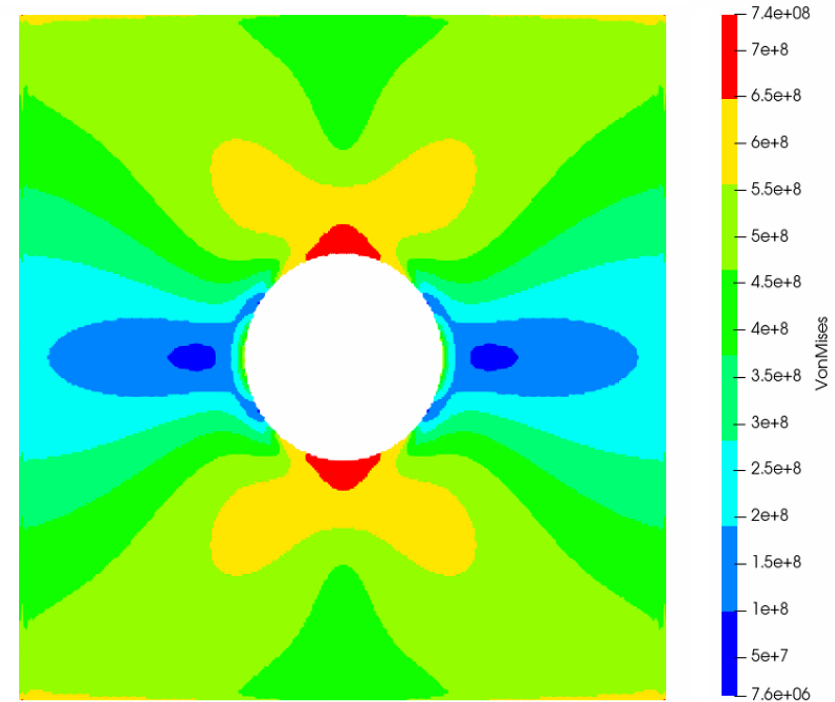
Kinematic hardening



Mixed hardening



Von-mises stress when $u_x = 0.125$ mm



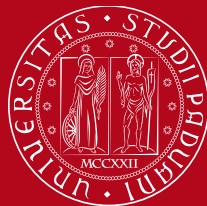
Von-mises stress when $u_x = 0.25$ mm

- A new **elastoplastic Peridynamic** formulation was developed for analysis of **materials** with **isotropic** and **kinematic** hardening.
- **Ordinary state-based Peridynamic** model was used for the first time to consider the effects of shear deformation in plastic domain for 3D cases.
- In comparison with the methods used before, the proposed method is able to consider deformations with **large rotations** and accurate values of **strain hardening** for each step.
- Dynamic relaxation method was used to obtain quasi-static solutions of nonlinear Peridynamic equations.
- The elastoplastic Peridynamic approach will be used to study **crack propagation** in **elastoplastic materials**.

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Thanks for the attention

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